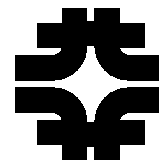




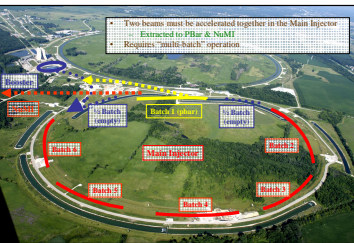
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# Cycle-to-Cycle Extraction Synchronization of the Fermilab Booster for Multiple Batch Injection to the Main Injector

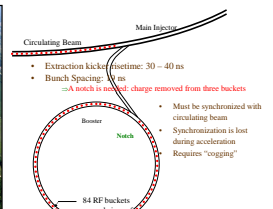


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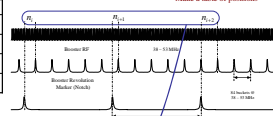


	Booster	Main Injector
Circumference (m)	474	3319
Harmonic Number	84	588
Kinetic Energy (GeV)	Injection 0.4 Extraction 8	Injection 8.9 Extraction 119
Momentum (GeV/c)	Injection 0.4 Extraction 8	Injection 8.9 Extraction 120
Frequency (MHz)	Injection 0.033 Extraction 52.8	Injection 0.033 Extraction 55.1
Acceleration Time (s)	0.033	0.7
Transition $\gamma_T$	5.45	21.8



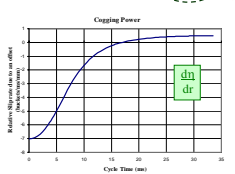
## Measuring Slippage

- Monitor Notch position throughout the cycle
- Use Main Injector RF as a standard clock
- Start counting on Main Injector revolution marker
- Stop Counting on Booster revolution marker
- Make a table of positions



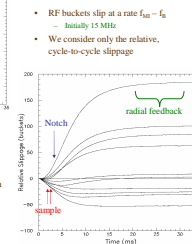
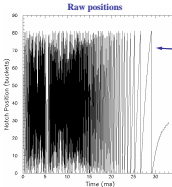
## Radial Feedback Concept

- Slippage can be induced by changing the radial position of the beam
- Changes the feedback of the Low Level RF system
- Changes the circumference
- Changes velocity
- Active feedback corrects error toward zero



## Notch Prediction

- Use the early part of the cycle to predict net slippage before extraction
- Place the notch anticipating further slippage (few ms into cycle)

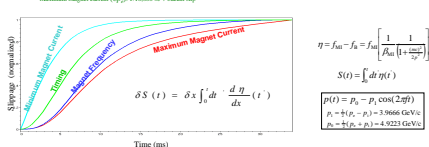


**Abstract**

We report on a system to ensure cycle-to-cycle synchronization of beam extraction from the Fermilab Booster accelerator to the Main Injector. Such synchronization is necessary for multiple batch operation of the Main Injector for the Run II upgrade of anti-proton production using slippacking in the Main Injector, and for the NuMI (Neutrinos at the Main Injector) neutrino beam. To perform this task a system of fast measurements and feedback controls the longitudinal progress of the Booster beam throughout its acceleration period by manipulation of the transverse position maintained by the LLRF (Low-level Radio Frequency) system.

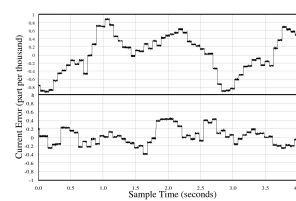
## Sources of Slippage

- Any change in the difference of frequencies ( $f_{\text{MI}}, f_B$ ) will cause slippage
- Some errors in the Booster can be parameterized as a change in  $p(t)$ 
  - Each has a particularly shaped slipper curve  $\delta S(t)$
- Several possible errors shown below:
  - Timing: 1  $\mu\text{s} \Rightarrow 15$  bucket slip
  - Magnet Frequency: 1 kHz  $\Rightarrow 1$  bucket slip
  - Minimum Magnet current ( $I_p$ ): 110,000  $\Rightarrow 10$  bucket slip
  - Maximum Magnet current ( $I_p$ ): 110,000  $\Rightarrow 7$  bucket slip
- Slip rate:  $h$  (buckets/time)
  - 15 MHz  $\Rightarrow 0$
  - $\Rightarrow 100 \Rightarrow 0.1$
- Total slippage:  $S$  (buckets)
  - $S_B = 100,000$  buckets
  - Only  $S_B$  and  $S_I$  is relevant
  - 1 part in 1000  $\Rightarrow 1$  turn



## Magnet Sag Correction

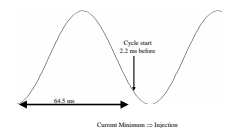
- Pulling of RF Anode causes injection current to sag
- Causes slippage variation by cycle in a cycle train
- Counter with feed forward compensation
- Half sine wave generated with clock



## Timing Errors

### Clock Error

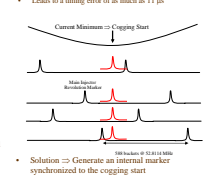
- Timing cycle start is predicted from previous cycle
- Small variation in 15 Hz frequency can lead to ms errors



- Solution  $\Rightarrow$  Trigger software off of magnet current level crossing instead of the cycle start

### Discrete Error

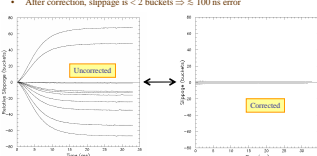
- Copping program starts on magnet minimum
- However, measurements are taken at MI markers
- MI markers come at arbitrary times w.r.t. minimum
- Leads to a timing error of as much as 1  $\mu\text{s}$



- Solution  $\Rightarrow$  Generate an internal marker synchronized to the copping start

## Timing Correction

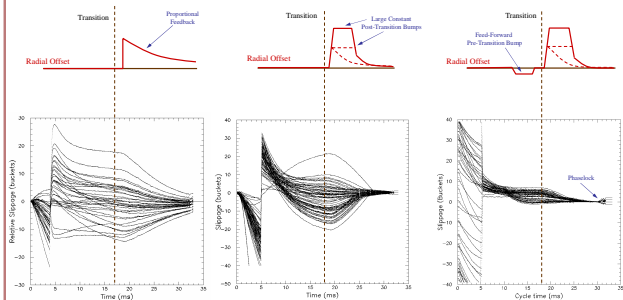
- Timing can be tested on cycles with no beam
- RF is generated by DDS and is identical cycle-to-cycle
- Slippage was consistent with a combined error of about 10  $\mu\text{s}$
- After correction, slippage is  $< 2$  buckets  $\Rightarrow \leq 100$  ns error



## Cogging Algorithms

- Algorithm has progressed to ensure cogging in the available time

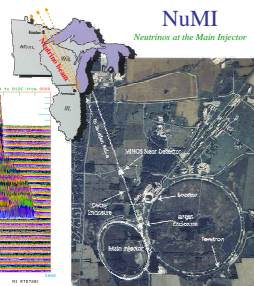
- Proportional (demonstration  $\leq 2003$ )
  - Radial feedback after transition proportional to error remaining
  - Needed to keep within maximum displacement
  - Decay time was too slow
- Flat & proportional (2004)
  - Small goes to proportional feedback
  - Constant larger than above
  - Larger errors go to a large constant value of feedback
  - Stay there until error is small
  - Return to proportional mode
- Pre-trans, flat, & enhanced proportional (2005)
  - Small pre-transition bump
  - Needs to use a prediction algorithm - like machining
  - Reduces post trans. cogging necessary
  - Flat feedback is the same as before
  - Proportional feedback is doubled when error is  $\pm 1$



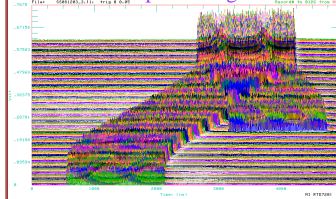
## Current Performance & Outlook

- Copping reduces extraction losses by 85-90 %
  - Ultimate performance: 90-95 % reduction
- Remaining Issue - Phaselock
  - Ruins cogging during synch to MI over last few ms
  - Irreducible error until new digital phaselock system is designed & implemented
  - Stopgap: Move extraction by 1-2 buckets cycle-to-cycle
  - Beams moves in MI, but probably okay

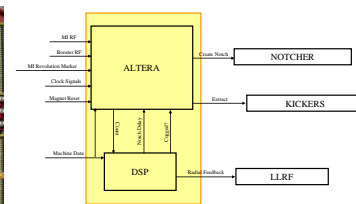
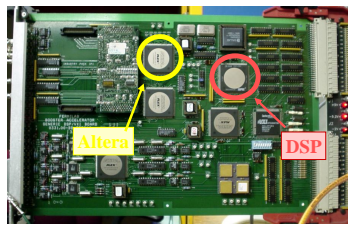
## Multi-Batch Applications



## Slip-Stacking

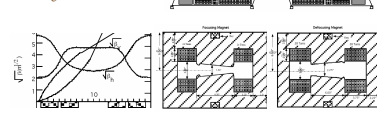


## Cogging Electronics



## Notching

- Kicker magnet knocks 3 buckets out
- Most of the beam is deposited into collimators
- Kicker must be large enough to scrape off beam
  - Beam is stiffer at higher energy
- Stronger PS needed



- Losses on cogged cycles show improvement with greater kick
  - Better cleans out notch
  - Reduces satellite bunches

